

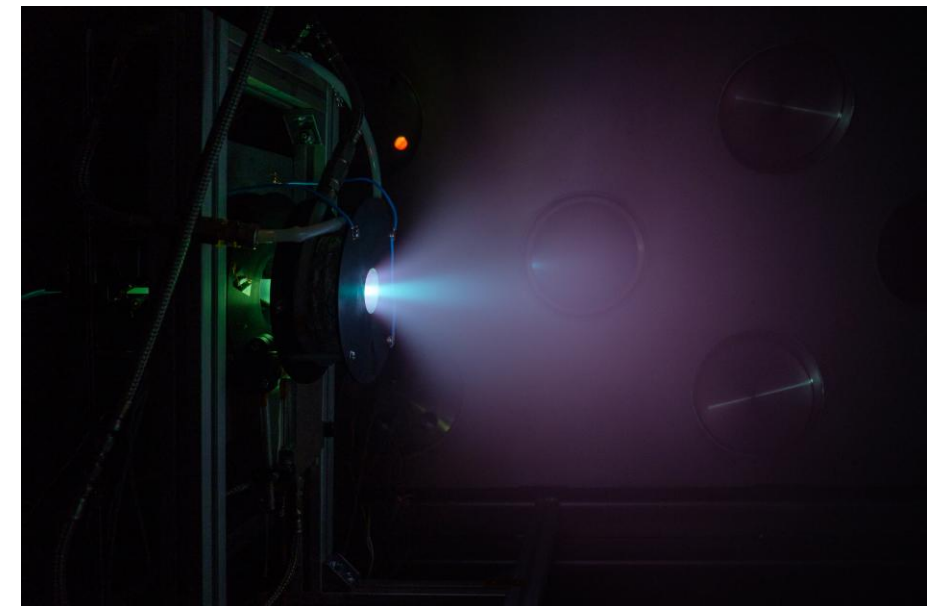
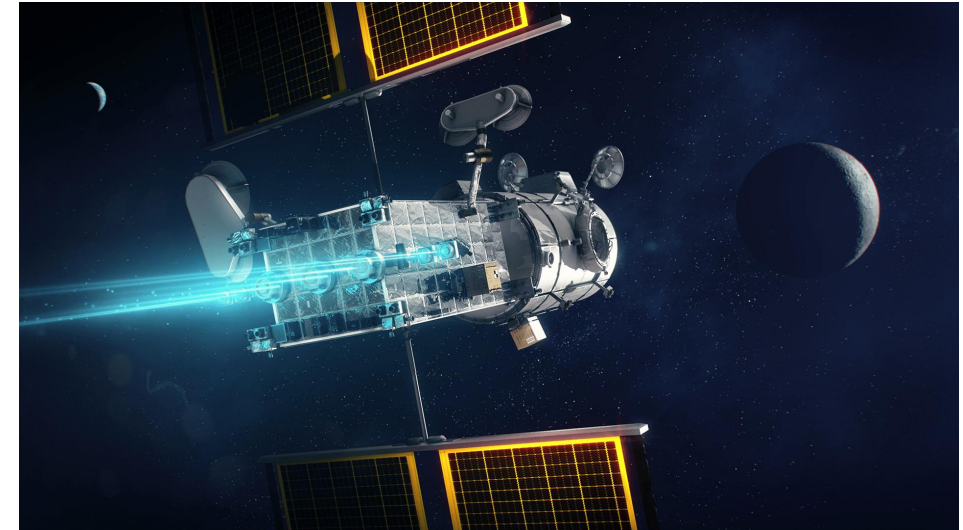
Experimental investigation of the physics of Electrodeless Plasma Thrusters for in-space propulsion

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Supervisor/s:
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PhD Aerospace Engineering UC3M
Doctoral Meetings 2026
2nd and 3rd June 2026

Problem statement: EPTs and efficiency

- Electric Propulsion is an established technology for satellite station-keeping, orbit raising, satellite de-orbiting
 - +10.000 of EP thrusters in orbit
- However, mature thrusters (HET, GIT) are constrained by:
 - Limited propellant flexibility
 - Reliance on cathodes for plume neutralization/plasma production
- **Electrodeless Plasma Thrusters (EPTs)** offer an alternative with several advantages:
 - Cheaper, simpler PPU
 - Propellant agnostic
 - Operational flexibility
- However, they are limited by their **low efficiencies**



$$\eta_T = \frac{T^2}{2\dot{m}P}$$

Thruster output

Thruster input

$$\eta_T = \eta_u \eta_d \eta_\epsilon$$

Thruster efficiency can be decomposed into three partial efficiencies

- Propellant utilization efficiency
- Beam divergence efficiency
- Energy efficiency

Problem statement: EPTs and efficiency

$$\eta_T = \frac{T^2}{2\dot{m}P}$$

Thruster output

Thruster input

$$\eta_T = 0.75 \cdot 0.5 \cdot 0.12 = 4.5\%$$

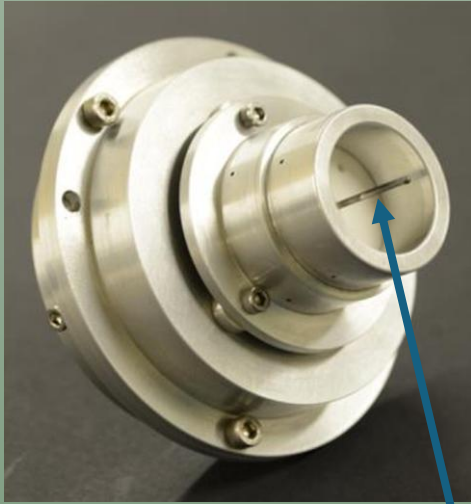
Thruster efficiency can be decomposed into three partial efficiencies

- Propellant utilization efficiency (30-75%)
- Beam divergence efficiency (35-55%)
- **Energy efficiency** remains the main bottleneck (4-12%)

- Inelastic collisional losses
- Particle/power lost to walls
- EM power reflected/radiated away

Poorly characterized
experimentally

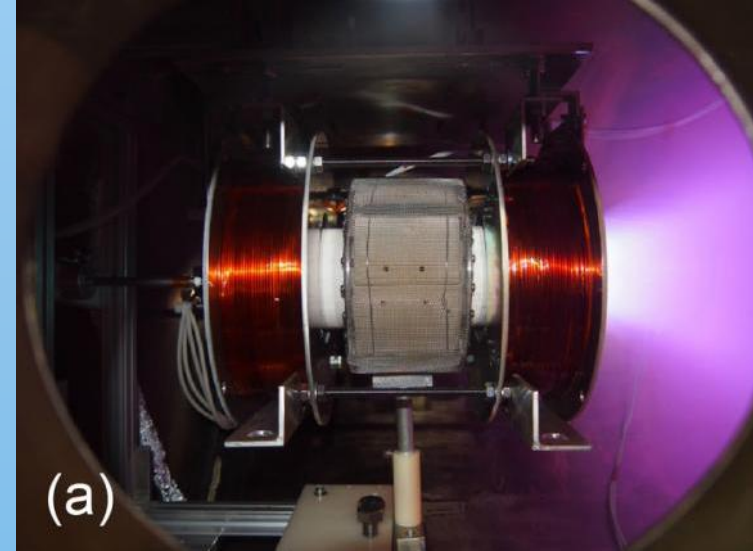
ONERA's ECRA



$$\eta_T \leq 50\%$$

(SoA)

Tohoku's University's HPT



$$\eta_T \leq 35\%$$

(this should be counted as an electrode btw...)

- Optimized through iterative design
- Poor attempts are made to explain what changed led to significant improvement
 - Not replicable by other groups
 - No lessons learnt

THESIS OBJECTIVES

Clarify main physical mechanisms governing plasma transport and wave coupling in EPTs and their MNs

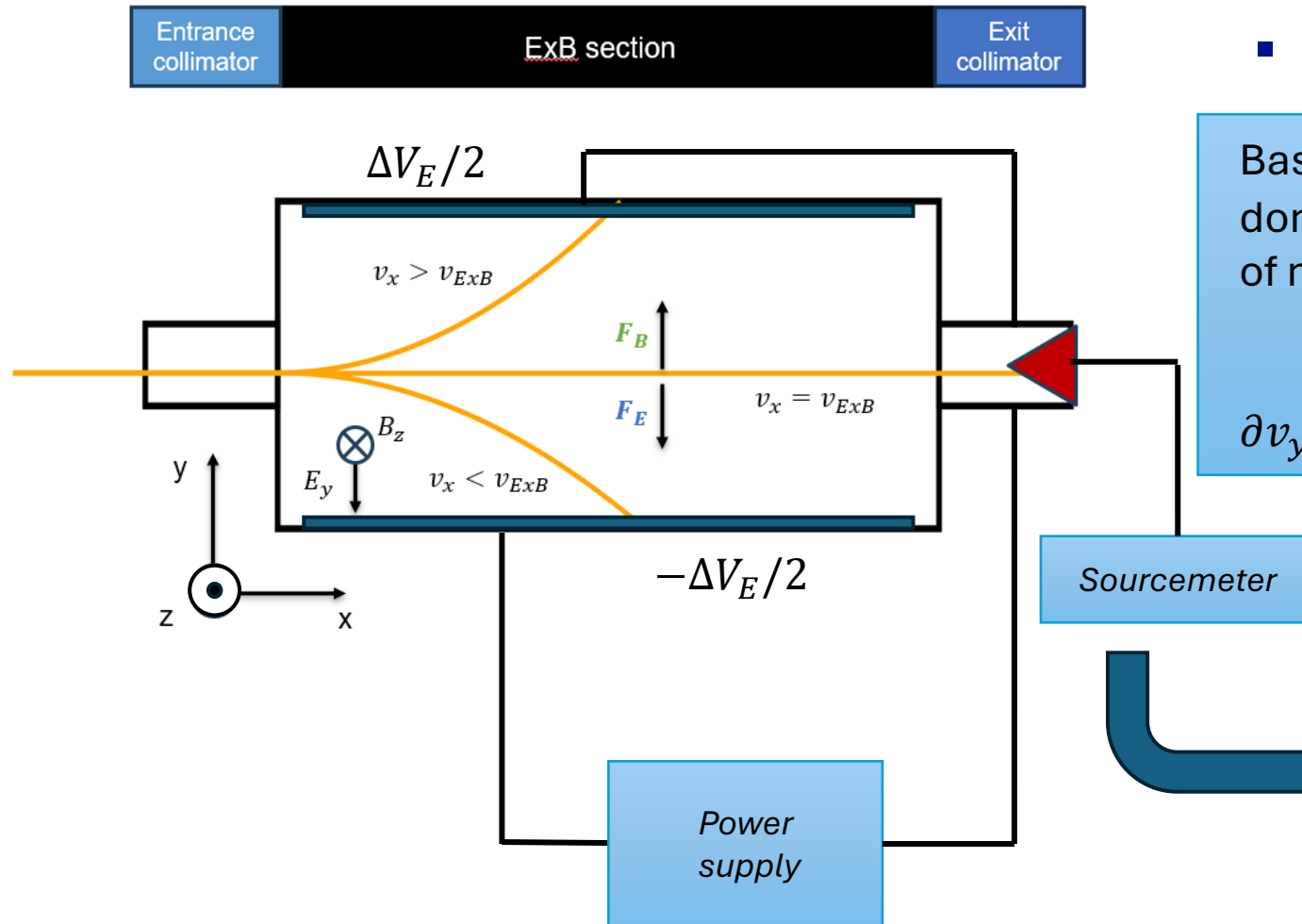
METHODS:

- Design, implement and/or use cutting-edge diagnostics, validated with existing ones
 - **ExB probe** → η_{ϵ}, η_u (energy lost by generation of multiply charged ions)
 - Laser Induced Fluorescence → η_{ϵ} (ion flux to the walls → wall losses)
- Develop digital twins of the diagnostics to relate measurements with plasma properties
- Characterize the EM wave energy loss pathways
- **By building physical models, propose ways to optimize existing EPTs**

Development of the EP2 ExB probe

$$v_{x,0} = \sqrt{\frac{Z}{m} e \Delta \phi_a} \propto \sqrt{\frac{Z}{m}}$$

- Why?
 - IVDF measurements needed for most of EP2 thrusters: ECRT, HPT (+air), CHT
 - Characterize multiply charged ions, plume composition
 - Correct thruster efficiency, also validate simulations
 - Gain experience in design, development and testing

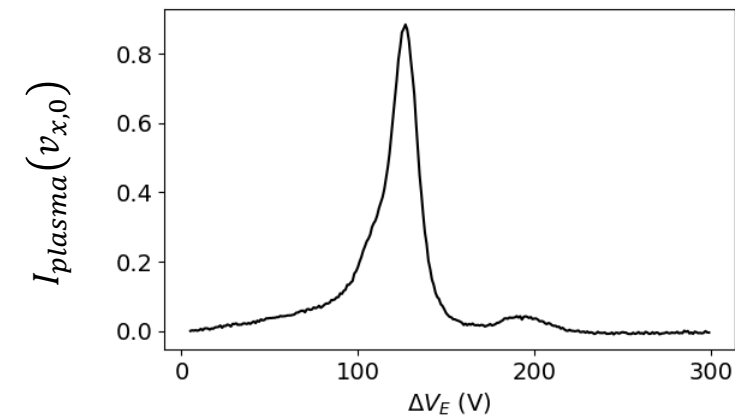


How?

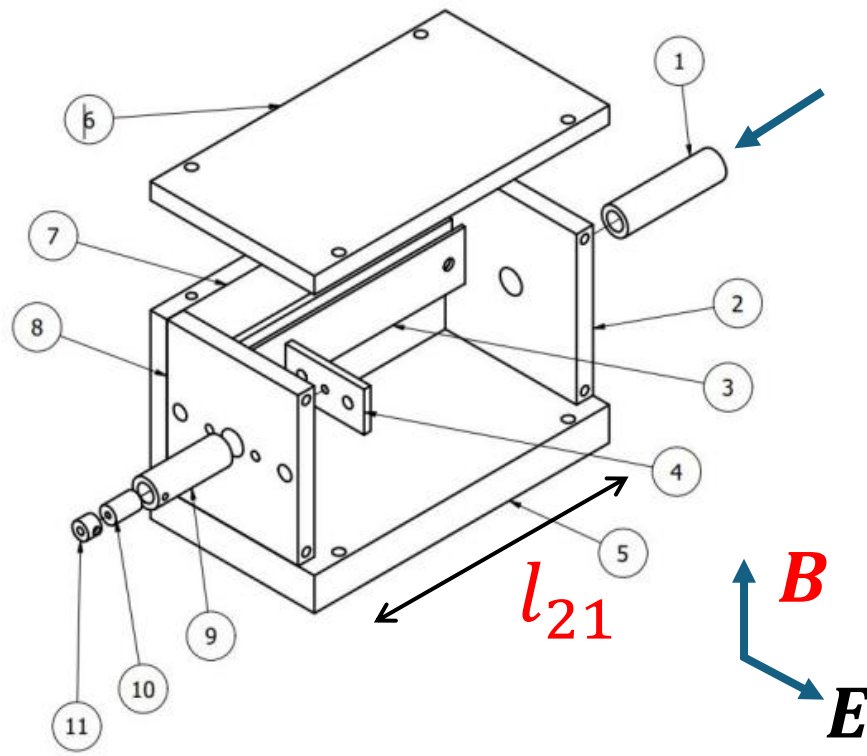
Based on crossed $\vec{E} = E_y \hat{y}$ and $\vec{B} = B_z \hat{z}$, the dominant term/component of a charged particle eq. of motion is

$$\frac{\partial v_y}{\partial t} = \frac{q}{m} (v_x B_z - E_y)$$

$\partial v_y / \partial t = 0$ if $v_x \equiv v_{ExB} = E_y / B_z$, the “ExB velocity”



$$I_{plasma}(v_{x,0}) = \sum_i Z_i e A_{coll} v_{x,0} f_i(v_{x,0}) \Delta v_{x,0}$$



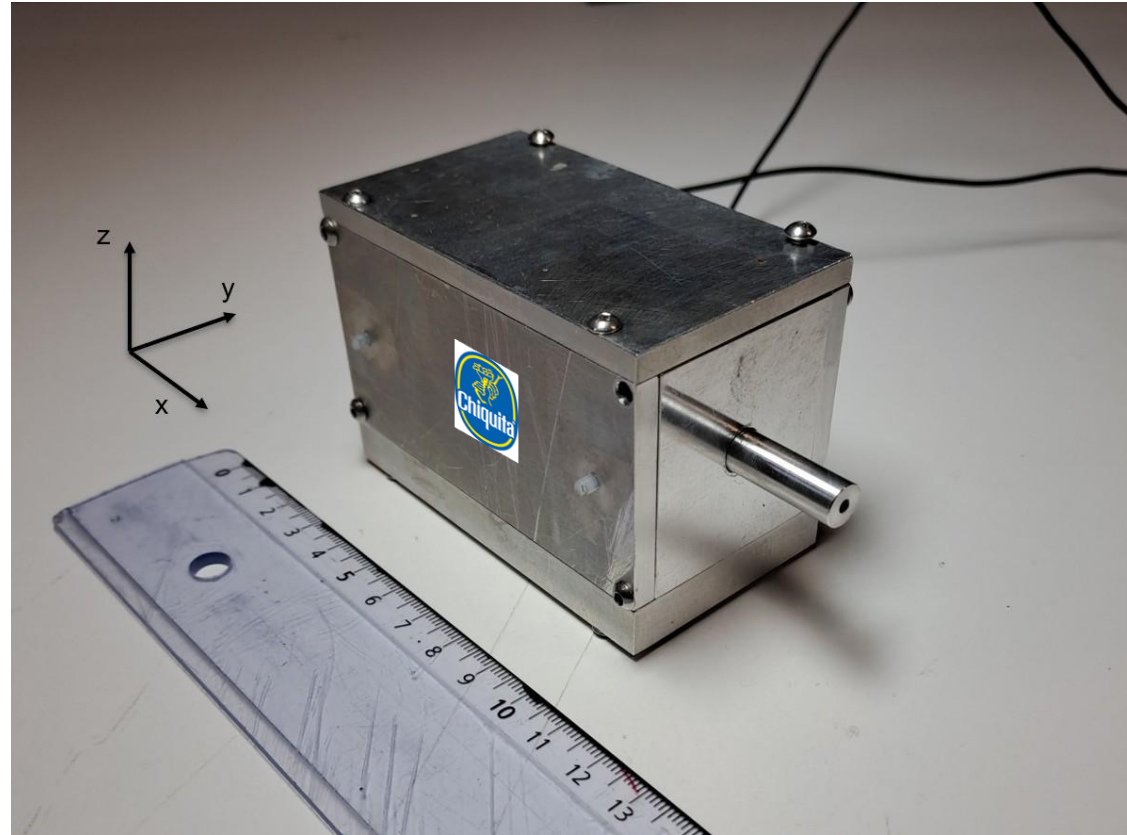
EP2 ExB probe

$$\delta v_x^g \sim 1 \text{ km/s}, l_{21} = 80 \text{ mm}, \\ B_z = 0.3 \text{ T}$$

- Design is mainly driven by the probe's "geometric" velocity resolution

$$\delta v_x^g = \frac{(d_1 + d_2)}{\mathbf{l_{21}^2 B_z}} 2\Delta\phi_a$$

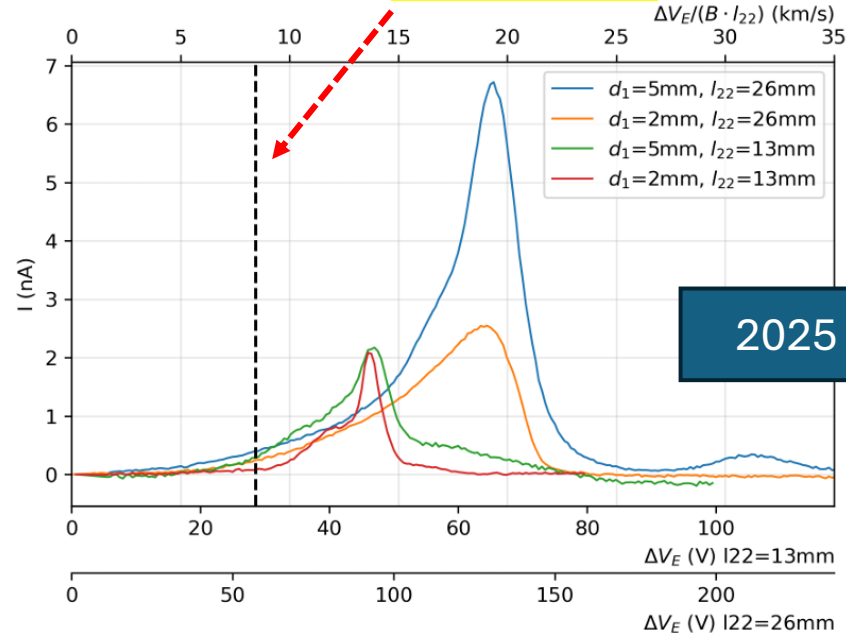
- For a given resolution, there is a balance between the probe's length and magnetic field strength
 - However, in the literature most probes share:
 - $l_{21} > 100 \text{ mm}$
 - $l_{11} + l_{21} + l_{31} \sim 300 \text{ mm}$
 - $B_z = 0.1 - 0.15 \text{ T}$
 - Can they be made **smaller**?
 - In principle, no scaling forbade this



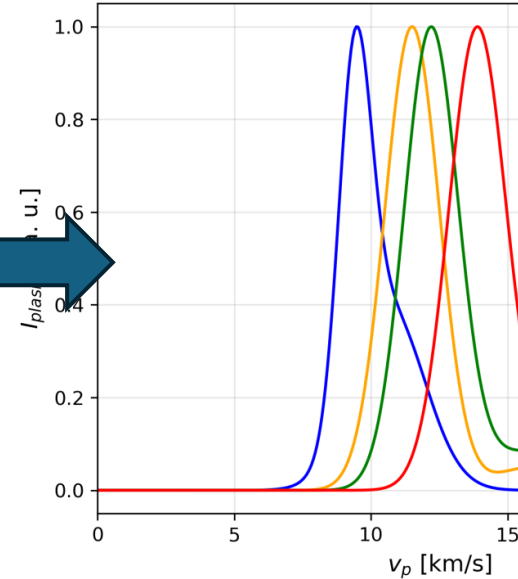
(Might be missing a better reference object, for scale)

1.5 years later

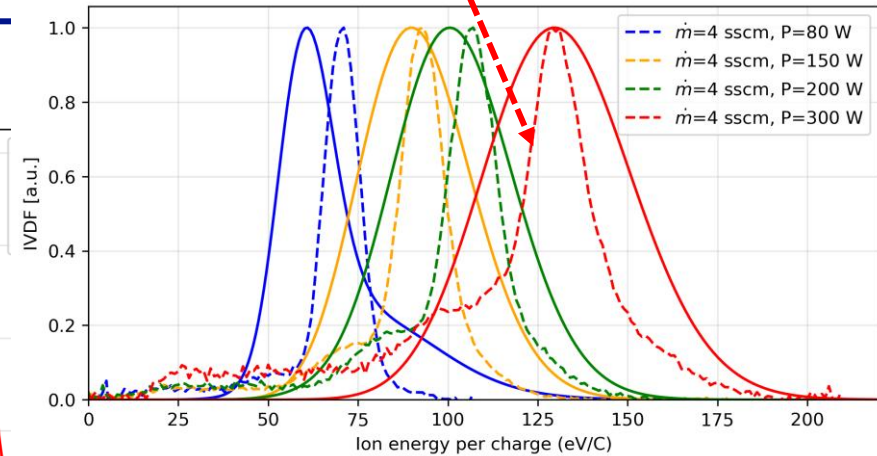
expectations



2025

 I_{plas} [a.u.]

expectations



2026

- Three main problems encountered when validating with other diagnostics
 - Velocity overestimated
 - Unexpected shape
 - Excessive broadening
- Seen across different probe configurations: understanding needed.

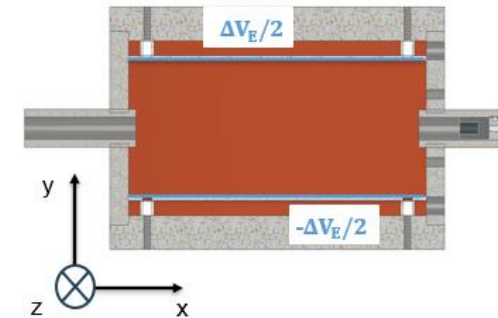
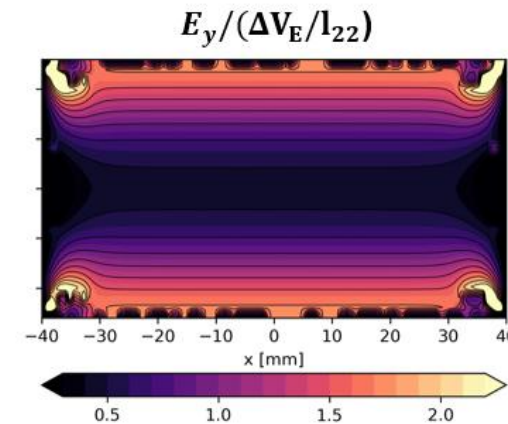
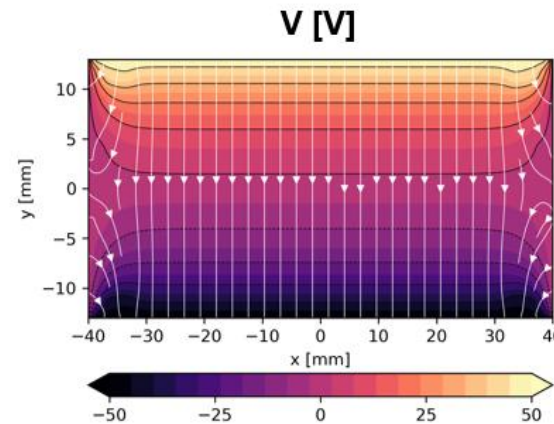
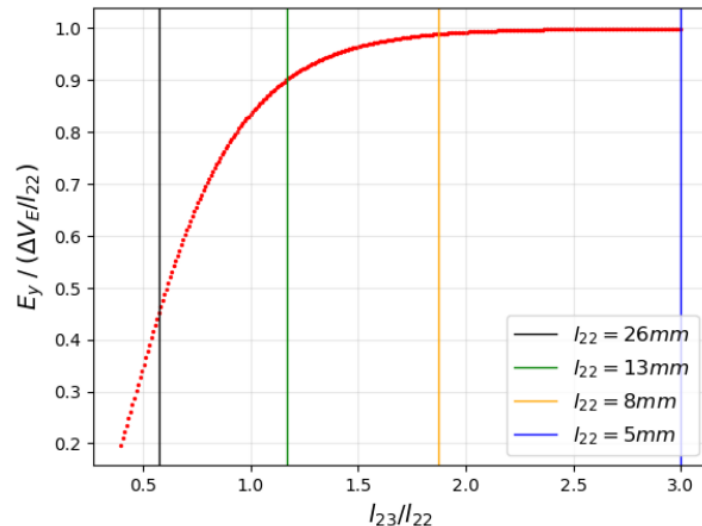
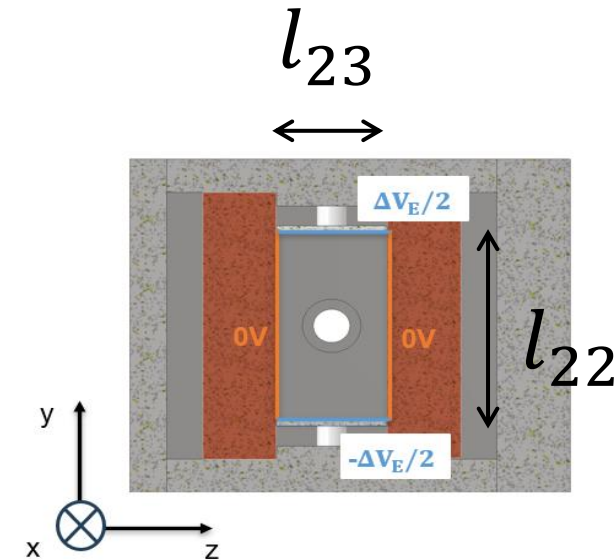


Towards a working probe

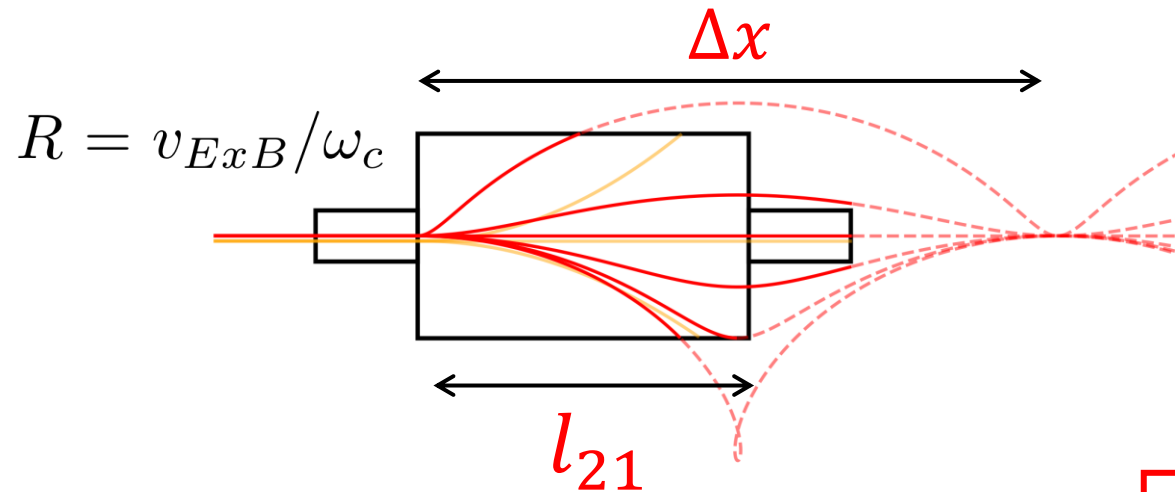
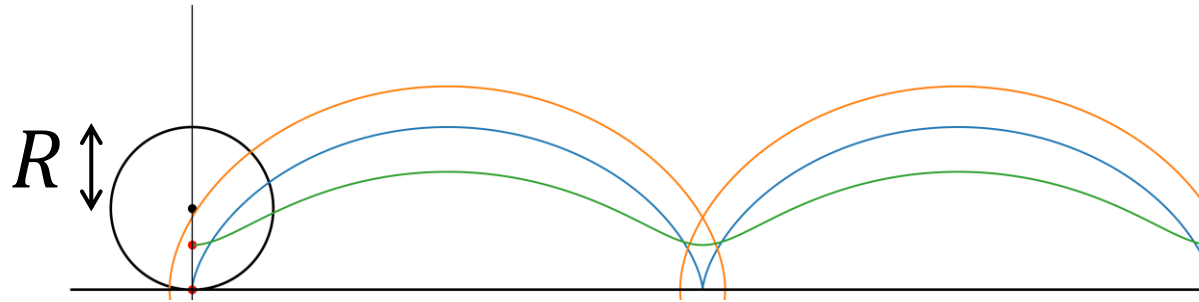
3 main problems

1st problem: overestimation of the particle velocity

- The small ExB dimensions makes electric field not uniform
 - Not just two parallel plates in a vacuum
 - Grounded magnets impose strong boundary conditions
 - If $E_y \neq \frac{\Delta V_E}{l_{22}} \rightarrow \mathbf{v}_{ExB}$ **incorrectly estimated**
- Lessons learnt:
 - Probe must have $l_{23}/l_{22} > 1.6$
 - (Should always simulate in 3D)



2nd problem: erratic measurements for low particle velocities



- If EoM are solved analytically, **trajectories are trochoid-like** (not ballistic)
 - Does not significantly affect results if $\Delta x < l_{21}$
 - However, below ΔV_E for which $\Delta x = l_{21}$, particle collection becomes erratic
 - Strong dependence on probe geometry
 - Under real fields, unpredictable. Reconstruction is not a possibility
- ExB probes **cannot* measure slow ions**
 - Ion speeds in EPTs are significantly lower than in GIT, HET

$$m_i \ddot{\mathbf{r}} = q(\mathbf{E} + \dot{\mathbf{r}} \times \mathbf{B}) = \begin{cases} m_i \ddot{x} = qB_z v_y \\ m_i \ddot{y} = qE_y - qB_z v_x \\ m_i \ddot{z} = 0 \end{cases} \rightarrow \begin{cases} x = \frac{v_{ExB} - v_{x,0}}{\omega_c} \sin(\omega_c t) + v_{ExB} t \\ y = \frac{v_{ExB} - v_{x,0}}{\omega_c} \cos(\omega_c t) - \frac{v_{ExB} - v_{x,0}}{\omega_c} \end{cases}$$

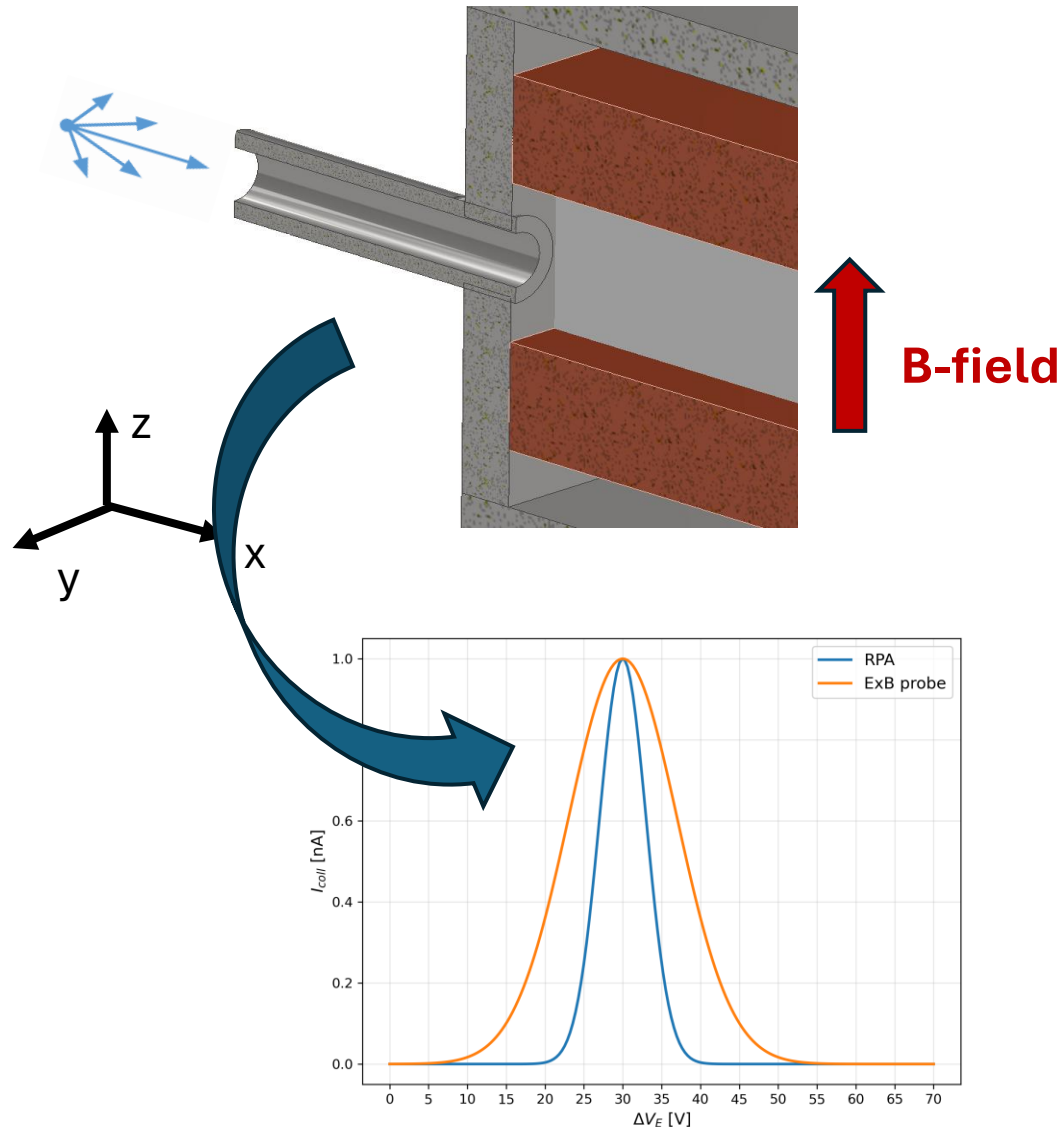
$\Delta x = 2\pi R < 2l_{21}$

$$\Delta V_E^{min} = ZeB_z^2 l_{21} l_{22} / m_i \pi$$

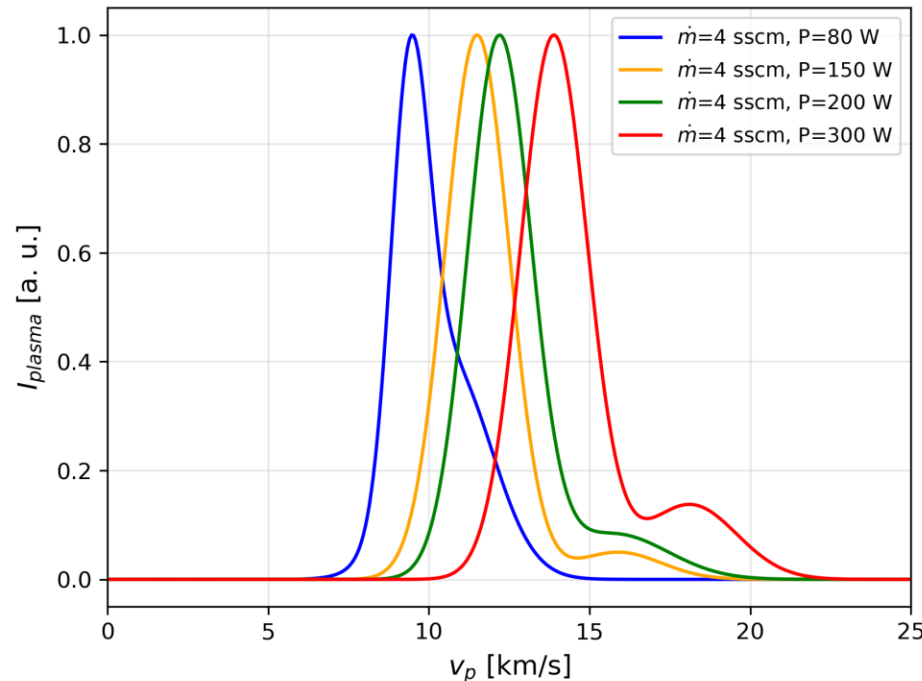
$$v_{ExB}^{min} = ZeB_z l_{21} / m_i \pi$$

- For our probe $v_{ExB}^{min} \approx 4.6 \text{ km/s}$ (Xe, Z=1)

3rd problem: artificial broadening of the IVDF



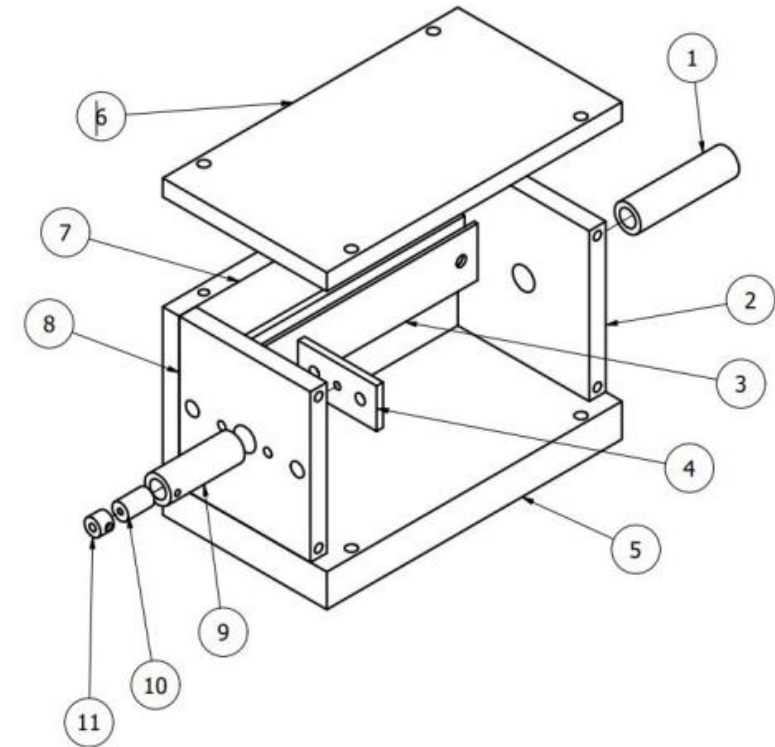
- What if something were making particles enter the probe at an angle?
 - Even when testing different collimator apertures, broadening remained
 - Plasma sheaths inside the collimator *may be* causing the observed broadening
 - $\lambda_{De} \approx 1 - 5 \text{ mm} \approx d_{coll}$
- Model developed for probe “angular response” supports this hypothesis



- Doubly-charged ($Z=2$) ions identified for the first time in the plume of a waveguide ECRT
 - As power increases, relative amount of $Z=2$ current becomes significant
 - Indicative of increasing density and/or T_e inside the source
- More certainty on the reconstructed spectra is needed to make further conclusions

Re-cap and next steps

- In the last year:
 - **Improved understanding** of ExB probe design and operation
 - **Expanded existing scaling laws** for the design ExB probes
 - Demonstrated the **existence of multiply charged ions** in waveguide ECRT
- Coming next:
 - Get measurements with a new entrance collimator to “fix” spectral broadening
 - Publish journal article with new design criteria, measurements in ECRT
 - Re-design EP2 ExB probe, **characterize plume of air-breathing HPT, CHT**
 - Survive (together with supervisors) rest of the thesis



- Presentation in Giessen Workshop on Plasma Diagnostics for EP
- **Bayón-Buján, B.**, Inchingolo, M. R., & Navarro-Cavallé, J. (2025). Challenges in the design of an ExB probe for Electrodeless Plasma Thrusters presented at the 39th International Electric Propulsion Conference (London, UK)
- **Bayón-Buján, B.**, Inchingolo, M. R., & Navarro-Cavallé, J. (2026). On the broadening of the Ion Velocity Distribution Function measured with ExB probes in Electrodeless Plasma Thrusters. Presented at the 10th Space Propulsion Conference (Bari, Italy)
- Published two articles from previous work
 - Maddaloni, D., **Bayón-Buján, B.**, Navarro-Cavallé, J., Merino, M., & Terragni, F. (2025). Low-frequency oscillations in the magnetic nozzle of a Helicon Plasma Thruster. *Plasma Sources Science and Technology*, 34(4), 045008.
 - **Bayón-Buján, B.**, Bello-Benítez, E., Zhou, J., & Merino, M. (2025). Data-driven analysis of anomalous transport and three-wave-coupling effects in an $E \times B$ plasma. *Journal of Electric Propulsion*, 4(1), 58.
- Lecturer in
 - Classical Mechanics for Aerospace Engineering (2nd year Bachelor, 1st semester)
 - The Conquest of Space (1st year Bachelor, 2nd semester)

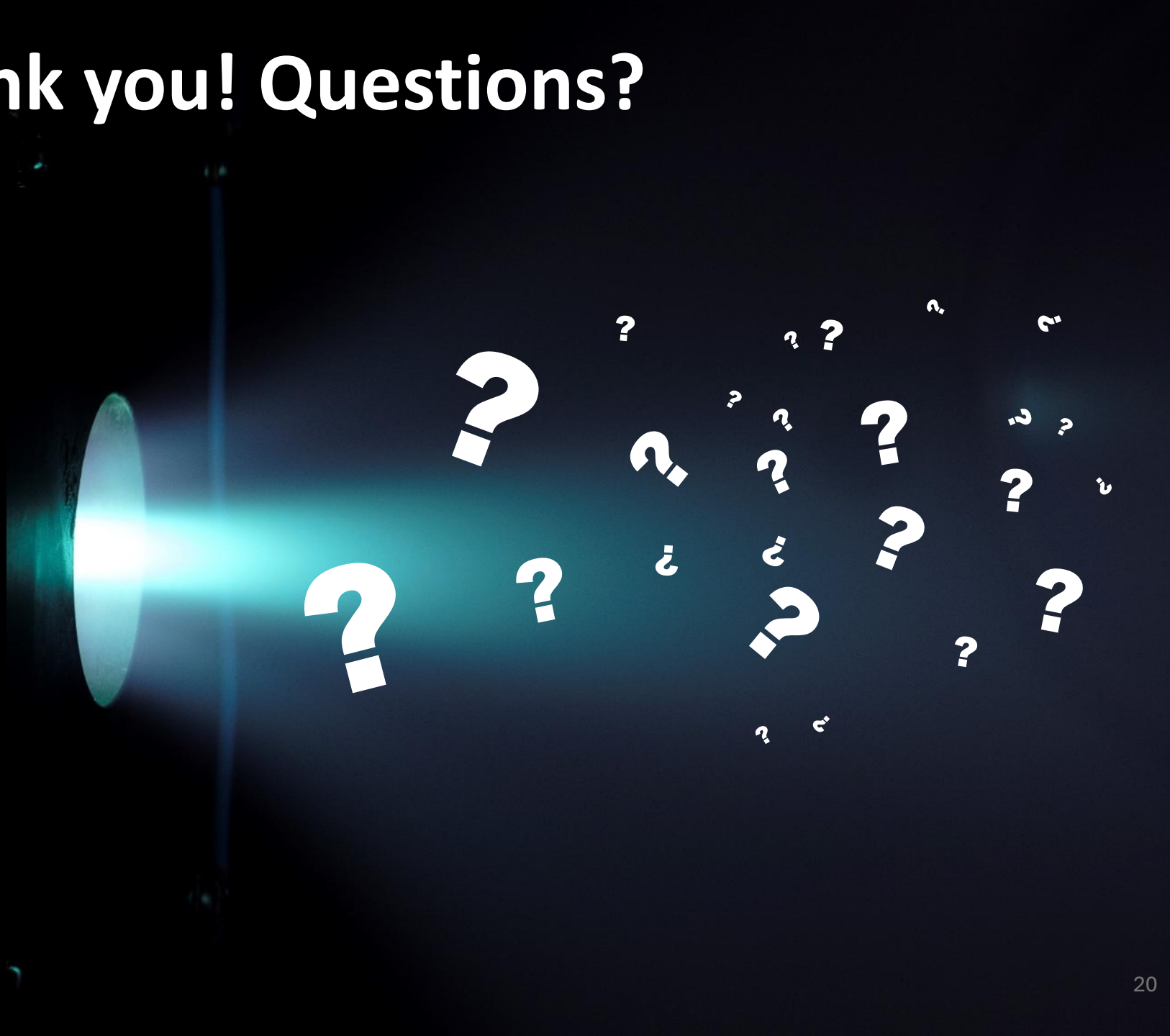
Thank you! Questions?

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EP² **uc3m**

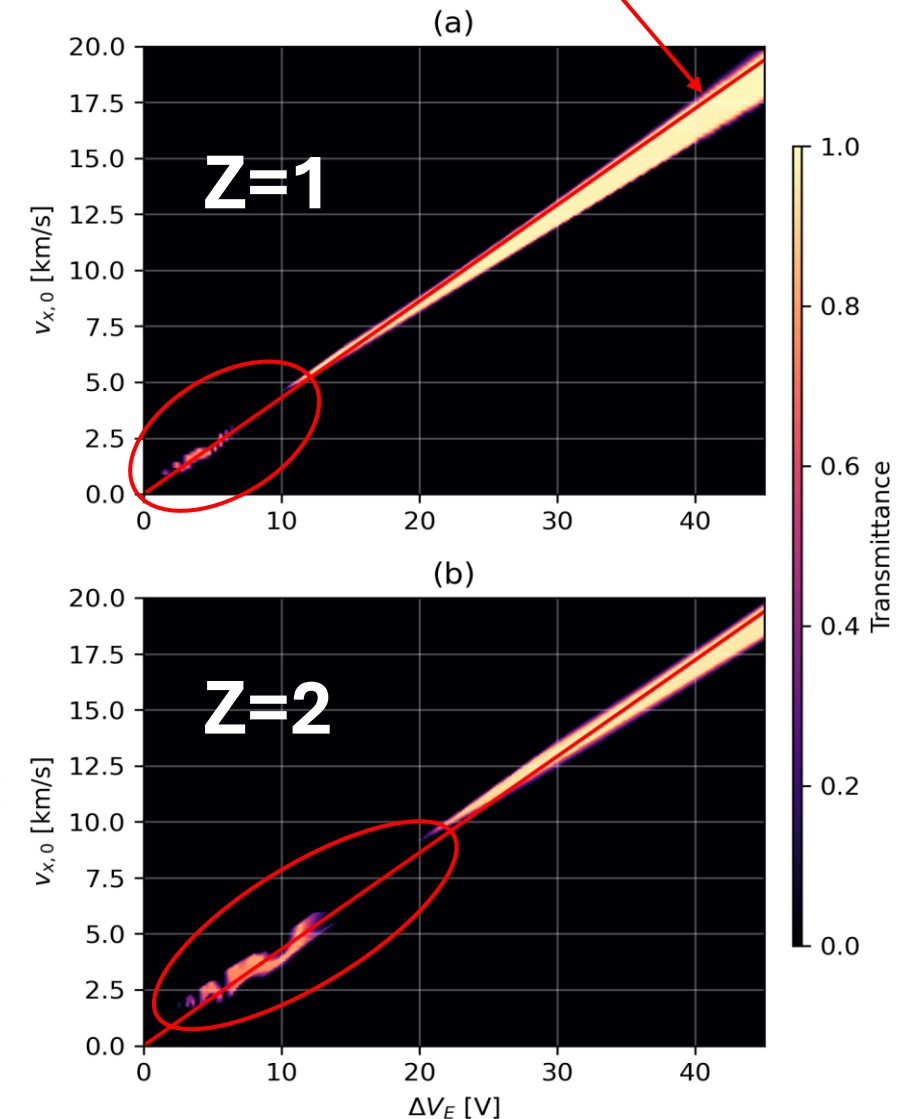
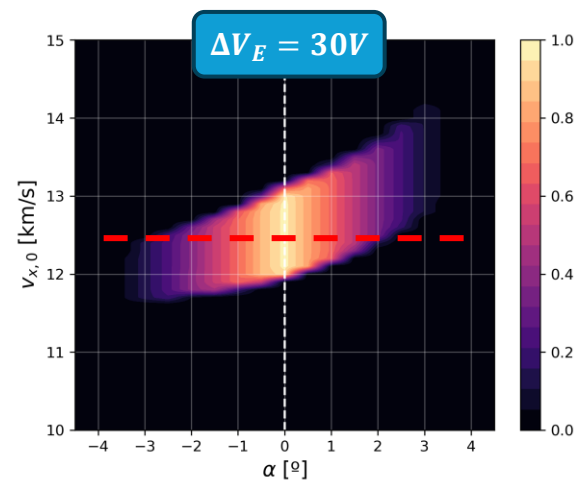
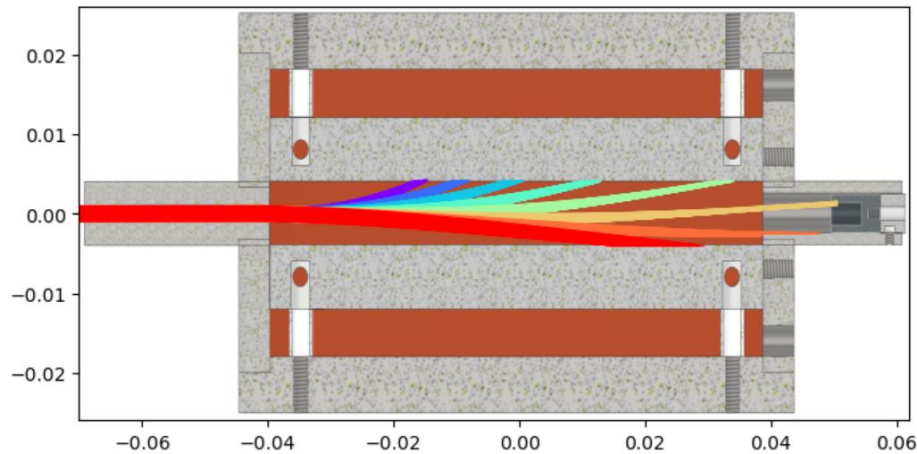


General framework: probe transmittance and IVDF reconstruction

- The measured $I_{coll}(\Delta V_E)$ is the result of convoluting the IVDF with the probe's transfer function: the **transmittance**

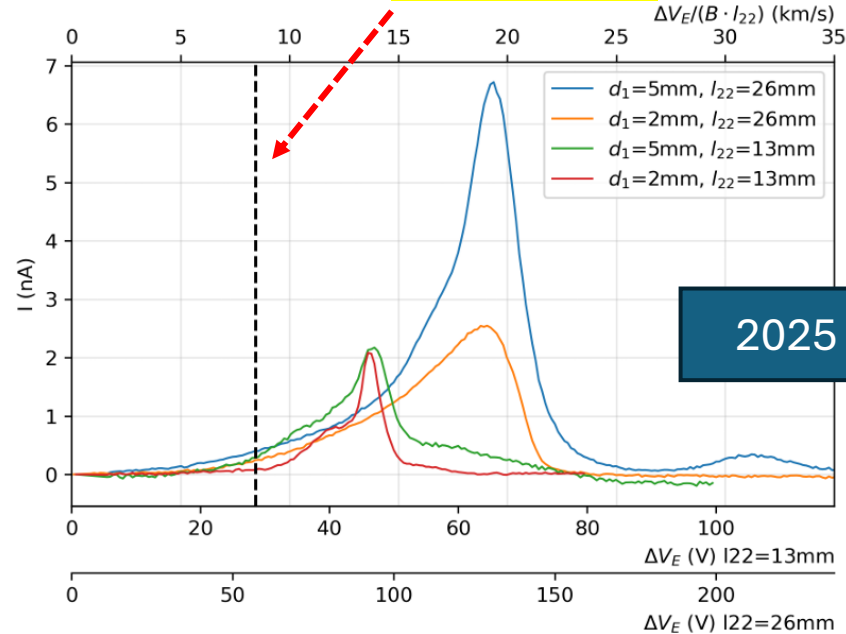
$$I_{coll}(\Delta V_E) = I_{plasma}(v_{x,0}) \otimes T(\Delta V_E, v_{x,0})$$

- Ideally, $T \sim 1$. As was seen, in general, not the case.
- T depends on probe geometry and fields.
- From the simulated transmittance, compared against the theoretical v_{ExB}
- Transmittance can be used to reconstruct $I_{plasma}(v_{x,0})$

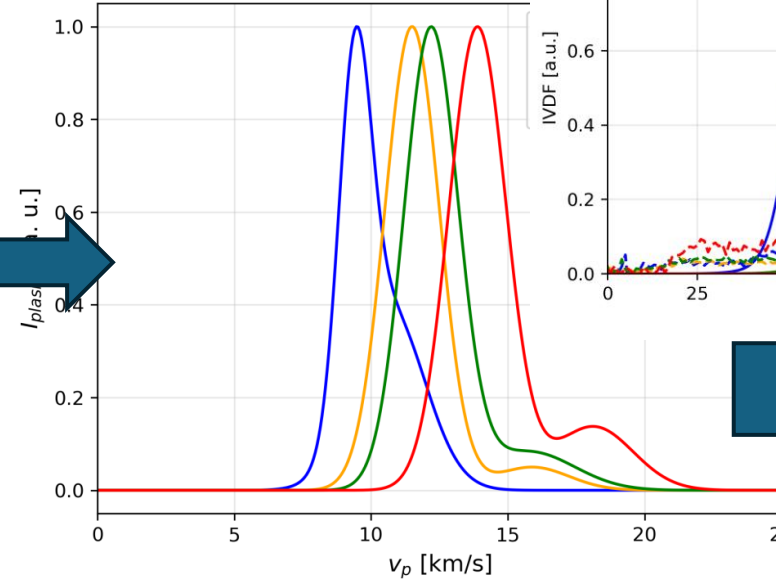


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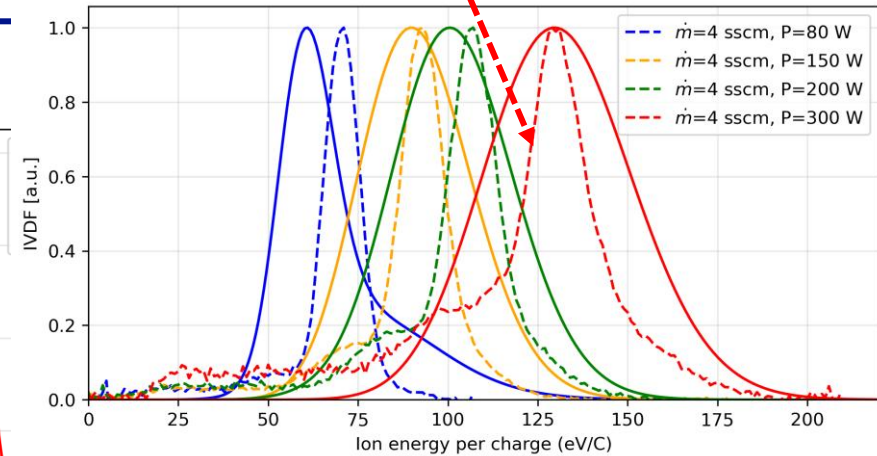
expectations



2025



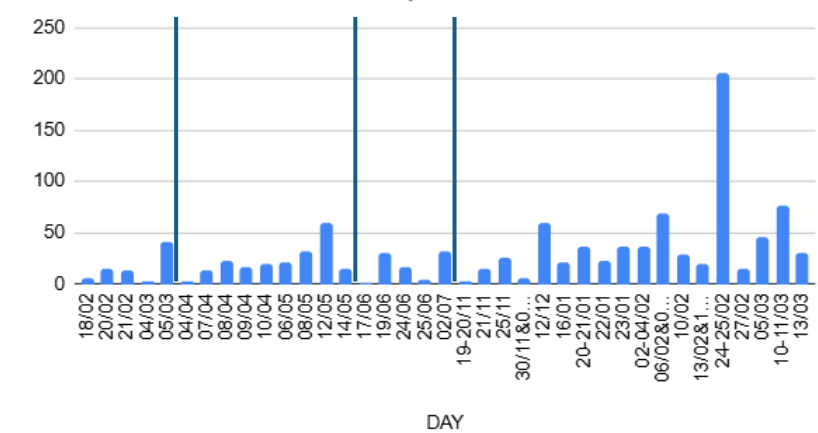
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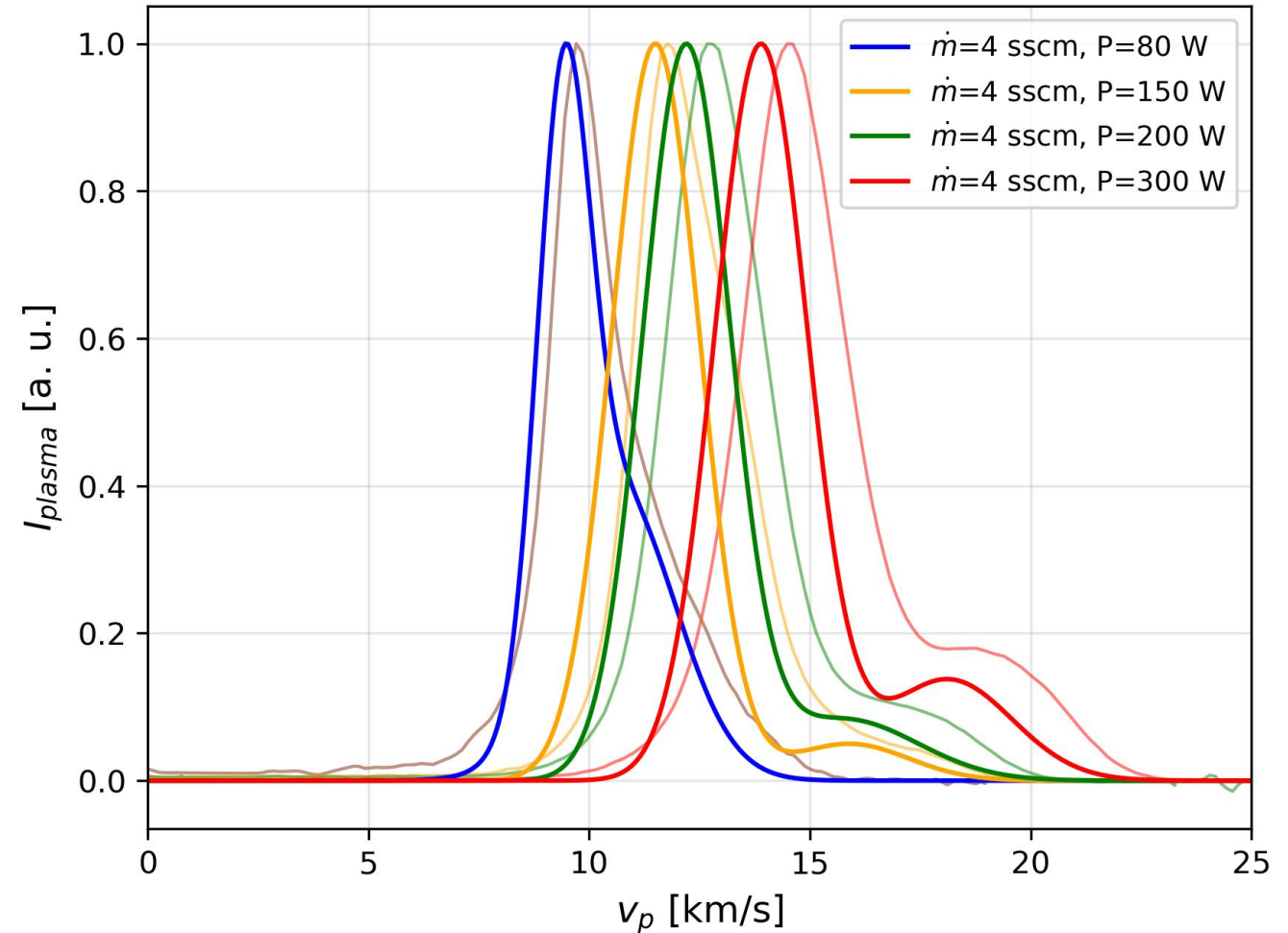
2026

- Carried out 4 separate experimental campaigns, **548 data points**
 - Spectra did not match expectations
 - Changed thruster type, propellant, operation point, probe configuration, position and orientation...
 - Carried out validation with other EP diagnostics (RPA, FC)
 - Learnt A LOT along the way
 - Simultaneously developing ExB probe simulations

Number of measurements performed



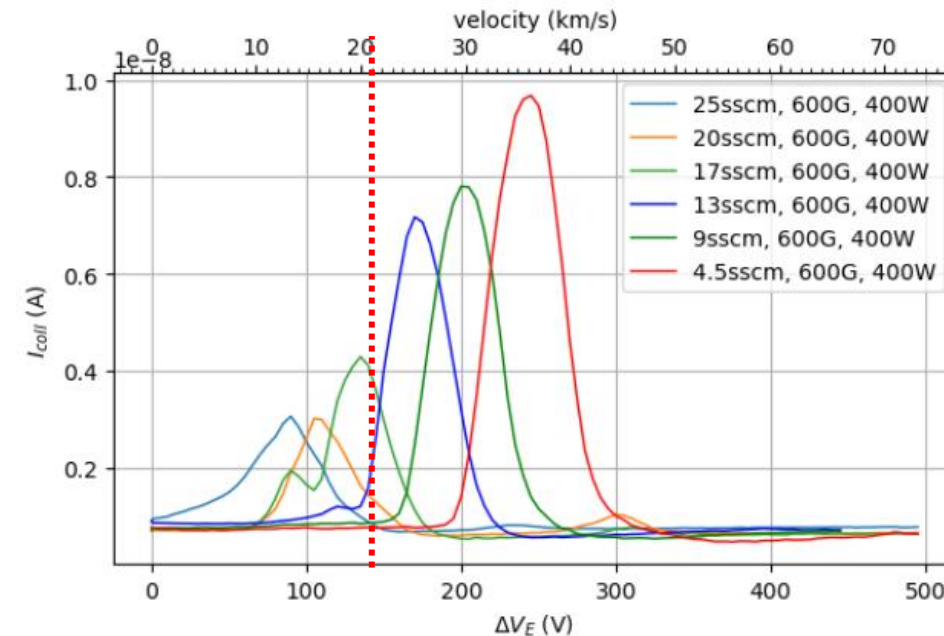
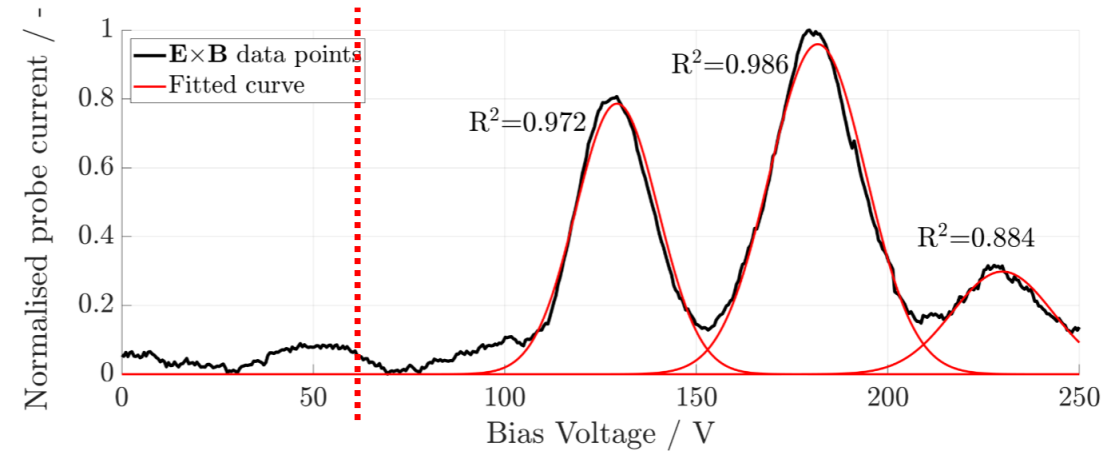
- Use of vExB can lead to severe (1km/s) velocity overestimation
- Doubly charged peak is also overrepresented



- Some examples on “trochoidal effects”

**Silvia Masillo and Andrea Lucca Fabris.

"Characterisation of the Halo Thruster: Plasma diagnostics and ground-test facility effects" IEPC25



$$\eta_F \approx \frac{F_{i\infty}^2}{2\dot{m}_p P_T} = \eta_u \eta_d \eta_e \eta_s,$$

$$\eta_u = \frac{I_i m_i}{\dot{m}_p e},$$

$$\eta_e = \frac{P_{i\infty}}{P_T},$$

$$\eta_d = \left(\frac{I_{zi}}{I_i} \right)^2,$$

$$\eta_s = \kappa_2^2 / \kappa_3,$$

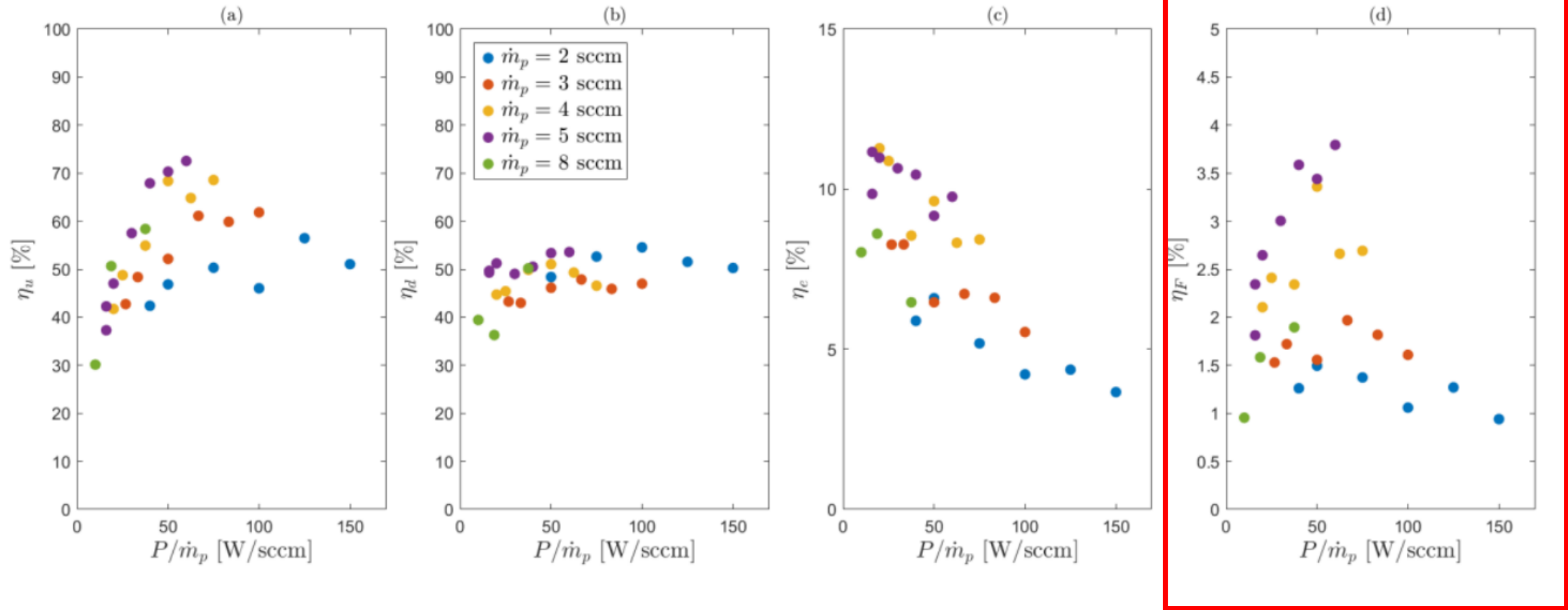
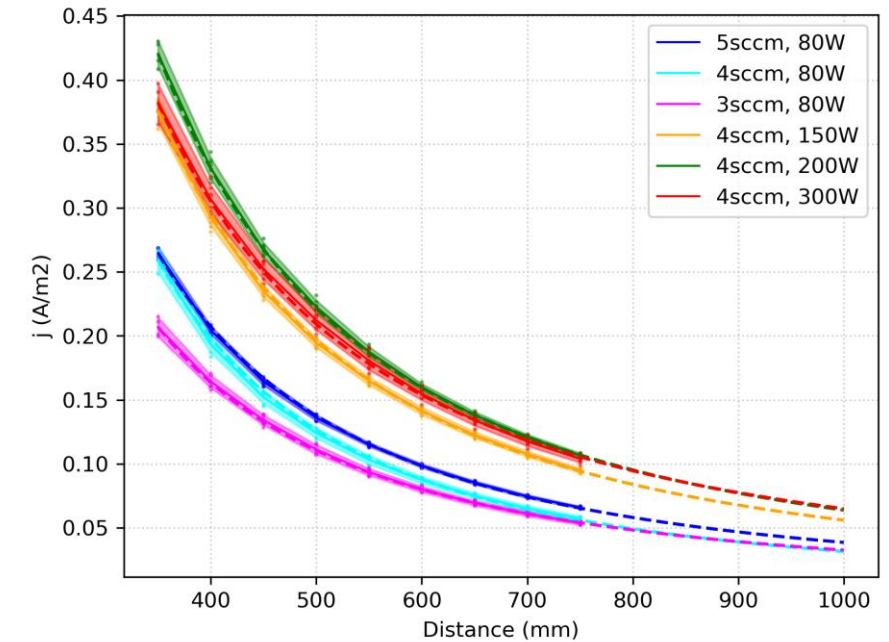
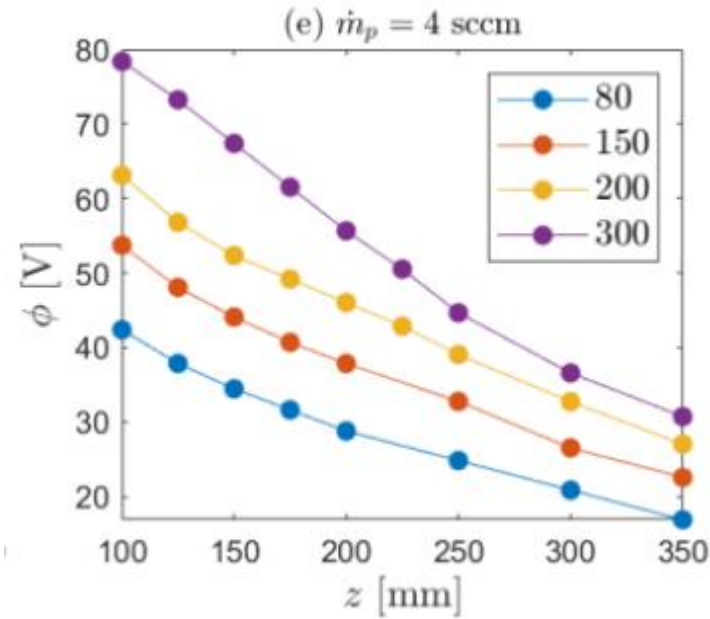
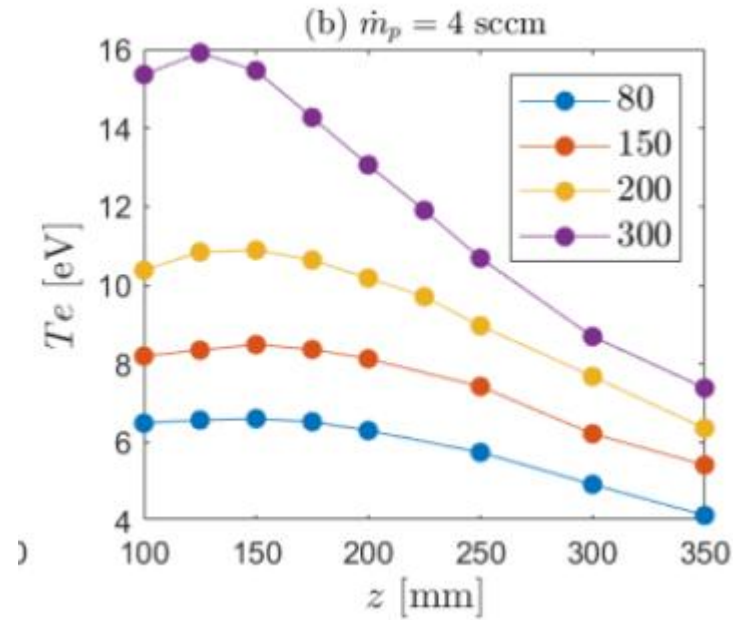
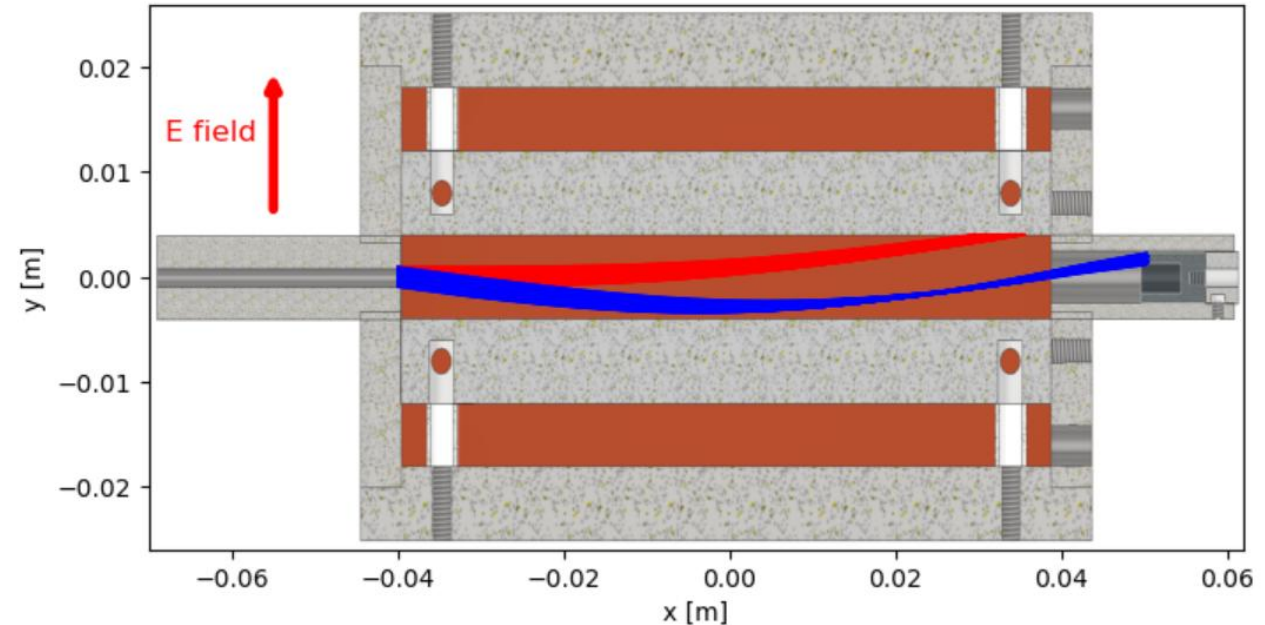


Figure 15. Partial efficiencies obtained with the Faraday cup and RPA measurements plotted against the power to mass flow rate ratio $P/\dot{m}_p$. (a), (b), (c), (d) are respectively the utilization η_u , divergence η_d , energy efficiency η_e and the thrust efficiency η_F .



- If particle inertia opposes the dominant force direction, particles with $v_x \neq v_{ExB}$ can be collected



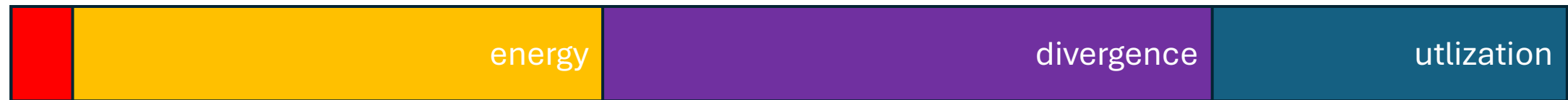
$$\Delta v_{ExB} = v_{x,0} - v_{ExB} = \frac{\Delta y - l_{21} \tan \alpha}{\frac{Z}{2} \frac{e B_z}{m_i} \left(\frac{l_{21}}{v_{x,0}} \right)^2}$$

Problem statement: EPTs and efficiency

$$\eta_T = \frac{T^2}{2\dot{m}P}$$

T^2 → Thruster output
 $2\dot{m}P$ → Operation point

$$\eta_T = \eta_u \eta_d \eta_\epsilon$$



“Remaining” thrust(er) efficiency (**useful power**)

$$\eta_T = 0.75 \cdot 0.5 \cdot 0.12 = 4.5\%$$

Thruster efficiency can be decomposed into three partial efficiencies

- Propellant utilization efficiency (30-75%)
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- **Energy efficiency** remains the main bottleneck (4-12%)

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experimentally